

REMARKS

Claims 1, 2 and 4 have been rejected under 35 U.S.C. §102(b) as being anticipated by Harris. Claim 3 has been rejected under 35 U.S.C. §103(a) as being unpatentable over Harris in view of Balk. Claim 5 has been rejected under 35 U.S.C. §103(a) as being unpatentable over Harris in view of Straumanis. Claim 6 has been rejected under 35 U.S.C. §103(a) as being unpatentable over Harris in view of Abe. Claims 7 and 8 have been rejected under 35 U.S.C. §103(a) as being unpatentable over Harris in view of LaSpisa. For the reasons that follow, Applicants traverse these grounds for rejecting these claims.

The device of the present invention is for producing bakery and confectionery products and, in particular, such products produced by extruding a dough compound or a sugar/fat compound. Applicants are not interested in obtaining protection for a device for extruding any other plastic compounds. In this respect all of the claims have been limited to the field of bakery and confectionery compounds. Applicants trust such a limitation will contribute to distinguishing the present invention over the prior art documents cited against this application. Applicants believe a sufficient basis for such a limitation can be found in the present specification, in particular at line 13 on page 3.

Furthermore, the present invention addresses a problem that is inherently involved when dough or sugar/fat compounds is being supplied by one or more roller presses, which, as mentioned at lines 13 to 15 on page 3 of the present specification, "owing to their design, provide an oscillating delivery pressure." The use of such a roller press as a feed instrument for extruding bakery and confectionery compounds of the kind specified above is further referred to from line 12 on page 8 of the present specification, and, in particular, in the last paragraph of that page and in the first paragraph of page 9.

Three examples of a roller press are disclosed in Altvater '233. The Examiner will note that in the embodiments shown in Figs. 1 and 2 each of the rolls 42, 44, 46 and 56 (Fig. 1) or 42, 44, 46 (Fig. 2) has a number of rotary bars 48 mounted thereto, each such bar defining a conveyor ridge and cooperating with a stationery strip 50 once in a revolution of the respective feeding roll. This is why pressure oscillations are inevitably generated as referred to in line 15 on page 3 of the present specification. The same applies to the embodiment shown in Fig. 3 of Altvater '233, wherein the feeding rolls 42, 44 and 46 have an undulated roll profile 60 each. The Examiner will appreciate that if the number of rotary bars or undulations on a specific feed roll is n , there will be n pressure oscillations per revolution of that feed roll.

It would appear that before the present invention was made, nobody ever bothered about such pressure oscillations simply because one had not recognized that certain undesirable non-uniformities of the extruded product were caused by such pressure oscillations. As a matter of course, it has been known to measure a product pressure at certain points of a roll-type press of the kind known from Altvater '233. However, the experts in the art had obviously either not noticed pressure oscillations occurring during each individual revolution of a feed roll in such a press, or had not believed that pressure oscillations during each revolution could have any detrimental effect on the uniformity of a product extruded through a nozzle fed by one or more such feed rolls.

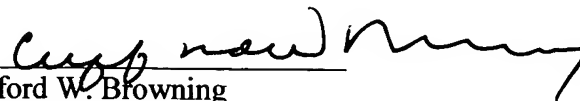
It would therefore appear that nobody had ever examined the possibility of compensating for pressure oscillations occurring during each revolution of each feed roll. It is true that Harris '589 discloses an extruder viscosity control system and method wherein, according to column 11, lines 7 to 9, minor variations in the throughput of a rotatable screw

14 may be compensated for by varying the speed of a gear pump 24 that is arranged between the rotatable screw 14 and an extrusion die 27. Whereas minor variations in throughput of such a rotatable screw may doubtless occur, such a rotatable screw certainly does not systematically generate pressure oscillations during each individual revolution thereof. Therefore, an expert considering Harris '589 would not have any reason to even think of compensating for pressure oscillations of the kind addressed in the present application.

Moreover, a gear pump 24 as proposed by Harris '589 is, in the light of the present invention, obviously not adapted to compensate for pressure oscillations of the kind addressed in the present application. As a matter of fact such a gear pump will inevitably generate pressure oscillations during each gear revolution, the number of such oscillations depending obviously on the number of teeth of each gear. Thus, although in Harris '589 the rotatable screw 14 does not generate, during each of its revolutions, any pressure oscillation, there will be pressure oscillations in the melt reaching the die 27, such oscillations having been caused by the gear pump 24.

For these foregoing reasons, Applicants request entry of the foregoing amendments to claim 1, reconsideration of the present application in light thereof, and allowance of amended claims 1-8 over all the prior art of record.

Respectfully submitted,

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Device for extruding plastic bakery and confectionery
products compounds

The invention relates generally to a device devices for
extruding plastic compounds ~~having the features mentioned~~
~~in the precharacterising clause of Claim 1;~~ and more
particularly to devices that extrude bakery and

5 confectionery products.

BACKGROUND OF THE INVENTION

Bakery and confectionery products are often produced by
extruding a plastic dough compound or sugar/fat compound.
In this case, the pressurised compound is extruded through
10 a die to form an extrudate. The extrudate itself may be cut
and/or removed by a conveyor belt. The external form of the
extrudate depends on the shape of the die and, in
particular, on the exit velocity of the compound from the
die. If the exit velocity of the compound fluctuates, then
15 the cut extrudate sections will differ in length, or the
extrudate on the conveyor belt removing it will be formed
with a non-uniform thickness.

DE-A-44 33 593 discloses a process for controlling an
extruder for foodstuffs, in which a viscosity sensor, which
20 determines measured variables such as the product
temperature, the pressure in front of the die, the specific
mechanical energy input, in particular the viscous
properties, and optionally also the dwelling time, is
installed between a worm tip and a die. The aim of the
25 process is to optimise and stabilise the working point of
the extruder. To that end, the rotational speed, the mass
flow rate and the water content are mentioned as
manipulated variables. In order to find the optimum working
point, functional relationships between the manipulated
30 variables and product criteria, such as colour, solubility
or degree of expansion, are firstly determined by running
various configurations on the extruder. Three further
control stages are subsequently carried out by using the
measured variables of the viscosity sensor.



WO 89/04610 discloses a process and an installation for making dough, in which a whirling mixer intimately mixes dry components with water and sends them in free fall directly to a kneading device. The kneading device delivers
5 shaped crumbly dough uniformly to two press screws, the feed to the individual press screws being controlled, in each case on the basis of the motor power consumption, as a function of the pressure in a press head. In order to prevent stagnation of crumbly dough in front of the press
10 screws, the latter have a higher delivery power than the kneading device. So that no air inclusions occur in the press screw, a vacuum space needs to be arranged between the kneading device and the press screw.

DE-A-22 15 449 and DE-A-43 14 728 each disclose a roller
15 press for extruding plastic compounds with two counter-rotatable rollers. The rollers have delivery strips, which revolve with the rollers and deliver the compound into a pressure chamber. The compound is separated from the rollers at a respective stripper and flows out of the
20 pressure chamber to exit dies. Such a roller press delivers the plastic compounds in pulses, since the compound is delivered more strongly by the delivery strips than in the spaces between two delivery strips. The pulsating delivery leads to a fluctuating exit velocity of the compound from
25 the exit dies.

The term "dough compound" means a mixture of different baking substances. These react with one another in the course of time, so that the dough compound can no longer be properly baked. This is referred to as "overageing" of the
30 dough compound. A dough compound can therefore be processed only up to a certain time after mixing.

Furthermore, when a dough compound is being processed, it is important that it should not be exposed to any large shear forces. Large shear forces break the adhesion of the
35 substances to one another, and individual substances, for example yeast cultures,

become damaged. The composition of the dough compound is therefore destroyed.

In a sugar/fat compound, large shear forces in the compound can lead to the segregation of fat. The composition of the sugar/fat compound is therefore likewise destroyed. The
 5 desired confectionery product can then no longer be produced.

SUMMARY OF THE INVENTION

It is an object of the invention to provide a device for
 10 extruding plastic compounds, in which the aforementioned disadvantages are avoided.

The object is achieved according to the invention by a device having the features of ~~Claim 1.~~ device (10) for extruding plastic compounds, having at least one feed
 15 instrument (12) for feeding a compound through a channel (24a; 24b; 24c) to a die (14), and a sensing instrument (60a; 60b; 60c) provided at the channel (24a; 24b; 24c) or at the die (14) in order to determine at least one measured variable (P_a ; P_b ; P_c) related to the viscosity of the
 20 compound, characterised in that the feed instrument (12) and the die (14) are configured in such a way that the feed instrument (12) provides a compound delivery pressure which oscillates over time at a frequency, and the die (14) has a flow resistance which oscillates at the same frequency.

25 For the extrusion of dough or sugar/fat compounds, roller presses are used which, owing to their design, provide an oscillating delivery pressure. Furthermore, in the case of rotatable dies, an oscillating fluctuation of the flow resistance of the compound in the die also occurs.

30 According to the invention, the two oscillating quantities are adapted to one another in such a way as to produce a substantially constant exit flow rate of the compound from the die. Alternatively, in the case of a non-rotating die, an instrument may be provided which adapts the flow

35 resistance of the die to the fluctuating delivery pressure

of the feed instrument, so that a substantially constant exit flow rate of the compound is likewise achieved.

Dough compound is an elastoviscous compound (Maxwell medium) which may be both viscous (Newtonian fluid) and
 5 elastic (elastic body). The viscous dough compound hence solidifies, for example, during baking, which is of course desired. Furthermore, however, the dough compound also solidifies during the processing time. From the consistency or viscosity of the dough compound, it is therefore
 10 possible to deduce whether the dough compound can, or should, continue to be processed. By virtue of the sensing instrument of the device according to the invention, it is therefore readily possible to detect whether a dough compound in the extrusion device is "overaged". Previously,
 15 this was not detected until at a downstream oven, so that fairly large amounts of waste were produced in the meantime.

The fat contained in a sugar/fat compound is a so-called non-Newtonian substance, i.e. it does not behave as a
 20 viscous compound. If the composition of the viscous sugar/fat compound is destroyed by large shear forces, fat is separated and the viscosity of the compound hence changes. Therefore, during the processing of a sugar/fat compound, it is also possible to detect, using the sensing
 25 instrument of the device according to the invention, whether the sugar/fat compound has the required composition.

According to an advantageous refinement of the device, the measured variable is the pressure of the compound. The
 30 following will be given as an explanation: for the flow of a viscous compound (Newtonian fluid) through a tube, the following applies

$$V' = [\pi R^4 (p_1 - p_2)] : (8 \eta l)$$

where V' is the volume flow rate of the compound, R is the
 35 tube radius, p_1 is the pressure of the compound at the tube

start, p_2 is the pressure of the compound at the tube end, η is the dynamic viscosity (consistency) of the compound and l is the length of the tube (see Hering et al.: Physik für Ingenieure [Physics for engineers] page 122, VDI-Verlag, Düsseldorf, 1989). When rewritten, this equation becomes:

$$\eta = [\pi \cdot R^4 (p_1 - p_2)] : (8 \cdot V' \cdot l).$$

Herein, R and l are constant. Furthermore, p_2 corresponds to the external pressure and can likewise be regarded as constant. If it is assumed that, at least for a certain time, the feed instrument feeds a constant flow rate V' into the tube, i.e. the die, then the pressure p_1 in the compound depends directly on the viscosity η . If the pressure changes, then this corresponds to a change in the viscosity of the compound and therefore, for example, to overaging of the dough compound.

The friction force F_R of the compound is equal to the pressure force F_P acting at the tube ends (ibid.):

$$F_R = F_P = (p_1 - p_2) \cdot \pi \cdot R^2.$$

This means that when the pressure p_1 in the compounded rises, the friction force F_R also increases. The pressure p_1 is therefore a measure of the friction force F_R of the compound. The friction force F_R depends on the flow resistance of the compound in the die and on the shear forces in the compound. As described above, the compound should not be exposed to large shear forces. With the aid of the determined pressure in the compound, it is then possible to limit the friction force on the compound and hence prevent its damage.

According to a further or alternative configuration of the device, the measured variable is the flow rate of the compound. According to the aforementioned equation

$$\eta = [\pi \cdot R^4 (p_1 - p_2)] : (8 \cdot V' \cdot l),$$

the viscosity η depends on the pressure p_1 and the volume flow rate V' . Through suitable means which limit the pressure p_1 , it is possible to keep constant the pressure p_1 prevailing in the die. The viscosity η therefore depends
 5 only on the volume flow rate V' of the compound. The volume flow rate V' of an incompressible fluid through a tube is

$$V' = \pi \cdot R^2 \cdot v_m,$$

where v_m is the average flow rate, or the exit flow velocity, of the compound. Determining the flow rate of the
 10 compound hence makes it possible to determine both the emerging volume flow rate and any change in the viscosity of the compound.

According to an advantageous configuration of the invention, the sensing instrument is coupled to a control
 15 instrument, and the control instrument is capable of controlling the feed instrument, as a function of at least one measured value determined by the sensing instrument, in such a way that the exit velocity of the compound from the die is not only substantially constant, but fluctuates
 20 minimally. The effect of a uniform exit velocity of the compound is that the bakery or confectionery products which are produced have a uniform shape and weight.

According to the above equations, the following applies:

$$V' = \pi \cdot R^2 \cdot v_m = [\pi \cdot R^4 (p_1 - p_2)] : (8 \cdot \eta \cdot l).$$

25 The average flow rate or exit velocity v_m can therefore be adapted by appropriately adapting the volume flow rate V' or the pressure p_1 in the die by using the feed instrument.

According to an advantageous configuration of the device according to the invention, it comprises a transport
 30 instrument for removing the compound extruded from the die, the sensing instrument being coupled to the control instrument, and the control instrument being capable of controlling the transport instrument, as a function of at least one measured value determined by the sensing

instrument, in such a way that the transport velocity of the transport instrument corresponds to the exit velocity of the compound from the die.

In the known devices, the transport velocity of the transport instrument is constant, so that a non-uniformly emerging compound, when arriving on the transport instrument, is stretched or compressed by the latter. According to the invention, the exit velocity of the compound and its removal rate are equal, so that a uniformly shaped compound extrudate is obtained.

According to a further advantageous configuration of the invention, the device comprises a rotary instrument having at least one rotatable die, the sensing instrument is operatively coupled to the control instrument, and the control instrument is capable of controlling the rotary instrument, as a function of at least one measured value determined by the sensing instrument, in such a way that the exit velocity of the compound from the die fluctuates minimally.

In the case of a rotatable die, the flow resistance of the die generally fluctuates during the rotation. The friction force F_R of the compound therefore changes. According to the above equations, however, it is possible to adapt the flow rate v_m of the compound as desired, by appropriately adapting the pressure p_1 in the compound by means of the feed instrument. This can be done, according to the invention, by using a control instrument.

In order to obtain bakery products with a plurality of extrudates, a feed instrument is connected through a plurality of channels to a die having a plurality of outlet openings, and a sensing instrument is in each case arranged at the channels or the outlet openings of the die.

The latter device is advantageously adjusted in the following way: the sensing instruments are operatively coupled to the control instrument, and the control

- instrument is capable of controlling the feed instrument, as a function of the measured values determined by the sensing instruments, in such a way that the exit velocities of the individual compounds from the outlet openings of the die fluctuate minimally relative to one another. By virtue of such uniformly emerging compounds, the layering of the bakery or confectionery products which are made has a constant thickness. The products therefore have an especially high level of dimensional and weight accuracy.
- 10 By using the device according to the invention, it is hence possible to make bakery or confectionery products with a much higher level of weight and shape accuracy than is the case with known devices.

BRIEF DESCRIPTION OF THE DRAWING

- 15 ~~The appended~~ Fig. 1 is a schematic drawing shows an exemplary embodiment of the device according to the invention for extruding plastic compounds, which will be explained in more detail below.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

- 20 A device 10 for extruding plastic compounds comprises a feed instrument 12, which is configured as a roller press and by means of which compounds, for example dough or sugar/fat compounds, can be fed to a die 14. A transport device 16 in the form of a conveyor belt is arranged below
- 25 the die 14. The emerging compounds pass, shaped into an extrudate, onto the transport instrument 16 and are removed horizontally by it. Bakery products are formed, for example, which are baked in a downstream oven (not shown).

- The extrudate may be cut or sealed by a cutting or pinching device (not shown), so that the cut sections of the extrudate are removed on the transport instrument 16. Furthermore, a plurality of dies 14 may be arranged next to one another, so that the capacity of the device is correspondingly enhanced.

- 35 For delivering and feeding the compounds, the feed instrument 12 has three pairs of rollers 18a, 20a, 18b, 20b

and 18c and 20c which, in a manner which is known and is therefore not described in detail here, receive the compounds from a respective supply line 22a, 22b and 22c. The rollers 18a to 18c and 20a to 20c have, distributed at
 5 the circumference, delivery strips which each deliver one compound into a respective pressure space (not shown).

During this, the delivery pressure generated by the delivery strips fluctuates according to the position of the delivery strips in the pressure space. The feed instrument
 10 therefore generates an oscillating delivery pressure which, in particular, fluctuates with the delivery rate v_a , v_b and v_c of the individual pairs of rollers.

When the rollers turn, the compounds are delivered with the feed pressure into channels 24a, 24b and 24c, respectively.
 15 The compounds reach the die 14, which is designed as a triple die and has three outlet openings (not shown). The outlet openings are arranged in such a way that the emerging compound forms an extrudate (not shown). The die 14 can be rotated with a rotational velocity v_d by
 20 means of a rotary instrument 26. The die 14 has asymmetrically arranged connection and ring channels (not shown) so that the compounds can flow from the channels 24a to 24c to the outlet openings even when the die 14 is turning. When the die 14 turns, differing flows pass
 25 through the individual connection and ring channels, so that the flow resistance of the compounds therefore fluctuates, and in particular this fluctuation oscillates as a function of the rotational velocity v_d of the die 14.

The rollers 18a to 18c and 20a to 20c can each be driven by
 30 a feed drive, these being operated by separately ventilated electric motors 28a, 28b and 28c, respectively. In this case, a respective temperature sensor 30a, 30b and 30c and hand switch 32a, 32b and 32c for manual operation is arranged at each of the electric motors 28a to 28c. The
 35 electrical supplies of the electric motors 28a to 28c are each provided with a respective frequency converter 34a, 34b and 34c and speed regulator 36a, 36b and 36c, by means of which it is possible to vary the rotational speed of the electric motors 28a to 28c and therefore the delivery rates
 40 v_a , v_b and v_c .

The rotary device 26 has a rotary drive, which can be driven by means of an electric motor 38. A temperature sensor 40 and a hand switch 42 are provided at the electric motor 38.

- 5 The rotational velocity v_d of the electric motor 38 can be adapted by means of a frequency converter 44 and a speed regulator 46.

The transport instrument 16 comprises a transport drive, which can be driven by means of an electric motor 48 with a
10 separately driven fan (not shown), a temperature sensor 50 and a hand switch 52. To regulate the rotational speed of the electric motor 48, and therefore a transport rate v_t of the conveyor belt, the electric motor 48 has an encoder 54, a frequency converter 56 and a speed regulator 58.

- 15 A pressure sensor 60a, 60b and 60c, respectively, is in each case arranged at the channels 24a to 24c, and, as a sensing device, is capable of determining the pressure p_a , p_b or p_c of the extruded compounds which prevails in the respective channels 24a to 24c.
- 20 The frequency converters 34a, 34b and 34c, 44 and 56, as well as the pressure sensors 60a, 60b and 60c are operatively coupled through lines (only partially shown) to a control instrument 62. The control instrument 62 is configured as a programmable logic circuit and can change
25 the delivery or feed rates v_a , v_b and v_c of the feed instrument 12, the rotational velocity v_d of the rotary instrument 26 and the transport rate v_t of the transport instrument 16 by means of the frequency converters 34a to 34c, 44 and 56, respectively.

- 30 In this case, the pressures p_a , p_b and p_c determined by the pressure sensors 60a to 60c are processed by the control instrument 62.

According to a first control method, the control instrument 62 in this case adapts the feed rates v_a , v_b and v_c in such
35 a way that the pressures p_a , p_b and p_c are constant, so

that, if the viscosity of the compounds remains the same, their exit velocity fluctuates minimally.

A second control method is configured in such a way that the transport rate v_t is adjusted to the exit velocity v_s of the emerging extrudate, so that the extrudate is not stretched or compressed when it arrives on the conveyor belt.

According to a third control method, the rotational velocity v_d is adapted to the delivery rate v_a to v_c , so that the fluctuating delivery pressure of the feed instrument 12 and the fluctuating flow resistance of the die 14 compensate for one another. For the revolution of n delivery strips of a roller during the time t , the rotational velocity v_d is selected in such a way that the die 14 rotates n times or with a multiple of n .

In a fourth control method, the delivery rates v_a to v_c are matched to one another in such a way that, depending on the viscosity of the individual compounds, pressures p_a , p_b and p_c prevail in the individual channels 24a to 24c such that the exit velocities of the compounds fluctuate only minimally relative to one another.

Alternatively, the pressure sensors 60a to 60c may be configured as flowmeters, the aforementioned control methods being appropriately adapted to the measured variable consisting of the flow rate, so that analogous control results are obtained.